# Speed of sound of oxygen in supercritical states up to 500 K and 100 MPa 

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#### Abstract

Oxygen is the second-most abundant element in the earth's atmosphere and plays an important role in various engineering applications. The precise knowledge of its thermophysical properties is thus important. As a fully fledged thermodynamic property, the speed of sound substantially contributes to the development and parameterization of equations of state. This work presents experimental speed of sound data for oxygen measured with an apparatus that is based on the pulse-echo technique with a double path-length. When working with pure oxygen at high temperatures and pressures, tight safety requirements have to be met, limiting the present measurements to 500 K and 100 MPa .


## Introduction

For optimizing industrial processes and for scientific applications the precise knowledge of thermodynamic properties is crucial. Oxygen, which is behind nitrogen the second-most abundant element in the earth's atmosphere, plays a major role in many industrial applications. The most accurate equation of state (EOS) for oxygen was established in the year 1985
by Schmidt and Wagner. ${ }^{1}$ Highly accurate thermodynamic property data from experimental measurements are the basis for developing EOS ${ }^{2}$ and speed of sound data are well suited for this purpose. However, there is a lack of speed of sound data in the supercritical region at elevated temperatures and moderate pressures, as illustrated in Fig. 1.


Figure 1: Experimental speed of sound data for oxygen: (•) Cook; ${ }^{3}$ (\#) Keesom et al.; ${ }^{4}$ $\left(\boldsymbol{)}\right.$ Bär; ${ }^{5}(\boldsymbol{+})$ van Itterbeek and Mariëns; ${ }^{6}(\times)$ van Itterbeek and Mariëns; ${ }^{7}$ ( $\square$ ) van Itterbeek and van Paemel; ${ }^{8}(\boldsymbol{\square})$ Liepmann; ${ }^{9}(\diamond)$ Galt; ${ }^{10}(\boldsymbol{\Delta})$ van Itterbeek and de Bock; ${ }^{11}$ $(\oplus)$ Boyer; ${ }^{12}(\boxplus)$ Verhaegen; ${ }^{13}(\mathrm{y})$ van Itterbeek and van Dael; ${ }^{14}$ ( $)$ van Dael et al.; ${ }^{15}$ (O) Blagoi et al.; ${ }^{16}(\nabla)$ Straty and Younglove; ${ }^{17}(\Delta)$ Baidakov and Kaverin; ${ }^{18}(\oplus)$ Abramson et al.; ${ }^{19}$ ( $ఔ$ ) this work.

Experiments with oxygen have been carried out by numerous authors and date back to the early 1900s, when Cook ${ }^{3}$ used Kundt's tube ${ }^{20}$ for speed of sound measurements of oxygen and air. First ultra-sonic measurements were accomplished in the 1930s, primarily in low pressure regions. Van Itterbeek and co-workers ${ }^{4,6-8,11,14,15}$ established an acoustic interferometer,
enabling for measurements with uncertainties of about $0.1 \%$. In 1938, Liepmann ${ }^{9}$ determined data for liquid oxygen using a light diffraction method for measurements at low temperatures. In the middle of that century, Galt, ${ }^{10}$ Boyer ${ }^{12}$ and Verhaegen ${ }^{13}$ contributed further data for low temperature and pressure regions. In 1962, van Itterbeek and van Dael ${ }^{14}$ used the pulseecho method in the liquid region between 64 K and 91 K and pressures of up to 92 MPa . Baidakov and Kaverin ${ }^{18}$ determined data with an uncertainty of $0.17 \%$ for superheated liquid oxygen for the first time in 1989, employing the pulse-echo technique by using an acoustic cell made out of glass. In 1999, Abramson at al. ${ }^{19}$ reached extremely high pressures of up to 12.6 GPa with a diamond-anvil cell, attaining an overall uncertainty of $2 \%$ in their measurements. An extensive study on the speed of sound of compressed liquid oxygen was presented by Straty and Younglove ${ }^{17}$ in 1973, employing the pulse-echo technique. An overview of these data is given in Fig. 1. The present work follows up on these measurements in a poorly sampled region, i.e. for temperatures between 300 K and 500 K and pressures between 40 MPa and 100 MPa . This region intentionally overlaps for one state point at 250 K and 34 MPa and for the 300 K isotherm over a pressure range from 10 MPa to 32 MPa with data by Straty and Younglove, ${ }^{17}$ cf. Fig. 2.

Speed of sound measurements of compressed oxygen in the supercritical state over a temperature range from 300 K to 500 K and a pressure of up to 100 MPa were carried out with the pulse-echo technique. ${ }^{21}$ The measurement principle was based on a sample cell that has two known propagation path lengths $l_{1}$ and $l_{2}$, where $l_{2}>l_{1} .{ }^{22}$ By emitting a modulated high frequency wave burst with a piezoelectric quartz crystal with a resonance frequency of 8 MHz , which was positioned between two reflectors in the fluid, the speed of sound $c$ was determined by the time measurement of the wave propagation through the fluid. Applying a Fourier Transformation based digital filter on the sampled acoustic wave signals increased their signal-to-noise ratio and enhanced their time and amplitude resolutions, improving the overall measurement accuracy. ${ }^{23}$ In addition, burst design led to technical advantages for determining the propagation time due to the associated conditioning of the echo. A
complete description of the method, apparatus and discussion of uncertainties has been published in preceding work. ${ }^{24,25}$


Figure 2: Comparison of speed of sound data for oxygen at 300 K measured by Straty and Younglove ${ }^{17}(\nabla)$ and in the present work ( $\hat{r}$ ) with the equation of state (EOS) by Schmidt and Wagner. ${ }^{1}$

## Safety requirements for handling oxygen

When working with pure oxygen, especially at high temperatures and pressures, tight safety requirements have to be met because it supports combustion and corrosion. Being highly oxidizing, it reacts vigorously with combustible materials and enhances fire or explosion, liberating large amounts of energy in a short time. A chemical reaction in an oxygen environment takes place, if the activation energy (i.e. ignition temperature) of a material is
exceeded. To prevent temperature peaks by adiabatic pressure surges, high fluid velocities through valves etc. of the apparatus should be avoided. Therefore, charging and discharging the measuring cell with oxygen through the piping system was done here very gently. Furthermore, the apparatus had to be free of welding beads and swarfs due to their sensitivity to pressure surges. ${ }^{26-28}$

The technical norm DIN EN 1797 introduces a method for testing the behavior of materials exposed to pressure surges, which can be caused by adiabatic compression or high gas velocities in pipes or components According to the recommendation BGR 500, ${ }^{26}$ which demands an appropriate steel alloy with an accumulated mass fraction of chrome and nickel above $22 \%$, the measurement cell was made out of highly corrosion resistant stainless steel (1.4571) and the cylindrical pressure vessel (sealed with a copper gasket) out of highly tensile steel (1.4462) that are both suitable for applications with pure oxygen

Pure copper has an ignition temperature of 1338 K in pure oxygen at $70 \mathrm{MPa} .{ }^{29} \mathrm{It}$ is even harder to ignite than stainless steel ${ }^{30}$ and is recommended in the literature as "particularly useful for resisting ignition by particle impact and therefore can be used in high-velocity gas applications for which burn-resistant alloys are required". ${ }^{28}$

The piezoelectric quartz crystal was connected by circular gold electrodes that do not hold any risks. The teflon coated cables were mechanically connected to the gold electrodes and on the other end soldered, without using any flux, to the electrical feed through. ${ }^{24}$ Upon combustion even small amounts of material may liberate large quantities of energy, resulting into an increasing temperature. This may lead to a chain reaction if the ignition temperature of other materials is attained. Thus, the lowest ignition temperature of all materials in the apparatus must not be exceeded Before use, the apparatus was very carefully cleaned and freed from impurities, especially of oily and greasy contaminants, which can induce a high risk due to their low ignition temperature. ${ }^{26,28}$

Before assembling all internal surfaces of the piping system including valves, both pressure sensors and the pressure cylinder were cleaned with acetone. After assembling, the system
was evacuated and then flushed about five times with argon at a temperature of 400 K . After a final evacuation, the system was flushed with oxygen for about one hour to minimize contamination by argon.

## Results and discussion

The measuring cell was filled at low temperatures of around 250 K , closed and then heated up to each studied isotherm. This isochoric pressurizing has a low risk of an increase of temperature through adiabatic compression by a feed pump or by a pressure surge in the piping system. Measurements were carried out from high to low pressure by releasing fluid to the ambient through a valve. Below a pressure of 5 MPa , measurements were not feasible due to the usual limitations of the pulse-echo technique, such as acoustic impedance and attenuation. These effects predominantly play a role in low density fluids, i.e., gases up to the critical region and other highly attenuating liquids, and impede the readability of the echoes due to their distortion, temporal extension and low amplitude. ${ }^{25}$

The first measurement was performed for a data point at 250 K and 34 MPa and showed a good agreement in a range of $0.07 \%$ with the data by Straty and Younglove, ${ }^{17}$ which is within the stated uncertainty. The overall uncertainty of the temperature measurement with a Pt 100 thermometer (Rössel Messtechnik RM-type) was less than $u_{c, \Delta T}=30 \mathrm{mK}$. The pressure was measured with two transducers (Honeywell TJE), one with a measuring range from 0 to 20 MPa and the second one with a measuring range up to 200 MPa . The first one had an uncertainty of $\pm 0.05 \%$ and the second one of $\pm 0.1 \%$ with respect to their full scale and therefore had a maximum absolute uncertainty of $\pm 0.2 \mathrm{MPa}$ above 20 MPa , which had the largest impact at low temperatures. This is a consequence of the pressure uncertainty, combined with the high isothermal compressibility of the fluid at such thermodynamic states. The propagation path lengths were referenced at the two isotherms 300 K and 350 K up to a pressure of 40 MPa with pure argon (cf. table 1.) using values calculated from the EOS
by Tegeler et al. ${ }^{31}$ with an uncertainty $u_{\mathrm{EOS}}=0.02 \%$. Here, the temperature was measured with the same Pt 100 thermometer which was used during the present oxygen measurements and the pressure was measured with a dead weight tester (DH-Budenberg 580 EHX) with an overall absolute uncertainty $u_{c, \Delta p, \mathrm{REF}}=0.02 \%$.

Table 1: Sample table.

| Chemical <br> Name | Source | Impurity | Purification <br> Method |
| :---: | :---: | :---: | :---: |
| Argon | Air Liquide | $\leq 10 \mathrm{ppm}$ | none |
| Oxygen | Air Liquide | $\leq 15 \mathrm{ppm}$ | none |

According to the error propagation law, the combined speed of sound measurement uncertainty $u_{c}$ is composed of the relevant contributions due to uncertainties of temperature (in this case twice, i.e. for referencing and measuring) and pressure measurements, as well as the uncertainties of the referencing procedure

$$
\begin{equation*}
u_{c}=\sqrt{2 \cdot\left(u_{c, \Delta T}\right)^{2}+\left(u_{c, \Delta p}\right)^{2}+\left(u_{\mathrm{EOS}}\right)^{2}+\left(u_{c, \Delta p, \mathrm{REF}}\right)^{2}} . \tag{1}
\end{equation*}
$$

The uncertainty of the operation procedure was limited by the internal time reference of the function generator and was thus neglected. Likewise the uncertainty of the very low impurity of oxygen (cf. table 1.) was not considered. Numerical experimental data together with their uncertainties are listed in table 2.

## Conclusion

The speed of sound of oxygen was measured in the supercritical region along five isotherms from 300 K to 500 K and from somewhat above 5 MPa up to 100 MPa . The measured speed of sound data for oxygen were compared with the EOS by Schmidt and Wagner. ${ }^{1}$ The uncertainties of the EOS which is valid in the temperature range from the triple point to


Figure 3: Absolute values (top) and deviations (bottom) of present experimental speed of sound data from the equation of state (EOS) for oxygen by Schmidt and Wagner ${ }^{1}$ at ( $)$ $300 \mathrm{~K},(\mathrm{O}) 350 \mathrm{~K},(\mathbf{\nabla}) 400 \mathrm{~K},(\Delta) 450 \mathrm{~K}$ and $(\mathbf{\square}) 500 \mathrm{~K}$.

300 K and a pressure of up to 80 MPa were stated as $1 \%$ for the speed of sound, except for the critical region. The present measurements confirm this uncertainty and show that for temperatures above 400 K the maximum deviation increases to about 1.6 \%, cf. Fig. 3. Steeper slopes of the isotherms at lower temperatures for the speed of sound as a function of pressure in the supercritical region can also be observed for other diatomic fluids like nitrogen (measurements by Costa Gomez et al. ${ }^{32}$ ) or hydrogen (equation of state by Leachman et al. ${ }^{33}$ ) at comparable states (cf. Fig. 3 (top)). Due to the large contribution of the pressure uncertainty (for measurements above 20 MPa around $95 \%$ and below 20 MPa around $40 \%$ ) to the overall uncertainty, $u_{c}$ has its maximum of almost $0.25 \%$ for the data point at 300 K and 30 MPa , cf. Fig. 3 (bottom).

This work covered a wide range of temperature and pressure in the supercritical state for which no experimental data were available for oxygen. The present results show that the pulse-echo technique is a reliable and accurate method for the measurement of the speed of sound of supercritical oxygen.

Table 2: Experimental data for the speed of sound of oxygen

| $T$ [K] | $p$ [MPa] | $c[\mathrm{~m} / \mathrm{s}]$ | $\pm u_{c}[\mathrm{~m} / \mathrm{s}]$ | $T$ [K] | $p$ [MPa] | $c[\mathrm{~m} / \mathrm{s}]$ | $\pm u_{c}[\mathrm{~m} / \mathrm{s}]$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 299.997 | 74.03 | 645.07 | 0.93 | 399.090 | 7.95 | 393.26 | 0.08 |
| 299.966 | 69.69 | 624.95 | 0.95 | 399.091 | 6.02 | 389.77 | 0.08 |
| 299.966 | 64.96 | 602.28 | 0.98 | 399.092 | 4.96 | 388.03 | 0.08 |
| 299.968 | 60.16 | 578.47 | 1.01 |  |  |  |  |
| 299.966 | 55.14 | 552.86 | 1.04 | 449.950 | 88.05 | 662.01 | 0.67 |
| 299.966 | 50.01 | 525.82 | 1.06 | 449.794 | 87.52 | 660.32 | 0.68 |
| 299.967 | 45.03 | 498.92 | 1.08 | 449.883 | 85.02 | 652.33 | 0.68 |
| 299.969 | 39.96 | 471.20 | 1.09 | 449.867 | 80.01 | 636.12 | 0.68 |
| 299.972 | 34.96 | 443.87 | 1.08 | 449.877 | 75.27 | 620.61 | 0.69 |
| 299.971 | 29.96 | 417.33 | 1.03 | 449.887 | 70.12 | 603.58 | 0.69 |
| 299.970 | 25.03 | 392.82 | 0.94 | 449.888 | 65.18 | 587.16 | 0.69 |
| 299.969 | 20.05 | 370.99 | 0.09 | 449.896 | 60.07 | 570.12 | 0.69 |
| 299.965 | 14.86 | 352.65 | 0.08 | 449.896 | 55.09 | 553.54 | 0.68 |
| 299.967 | 9.92 | 340.22 | 0.08 | 449.939 | 49.91 | 536.52 | 0.67 |
|  |  |  |  | 449.940 | 45.09 | 520.58 | 0.66 |
| 349.976 | 78.85 | 641.85 | 0.82 | 449.934 | 40.05 | 504.35 | 0.65 |
| 349.987 | 68.69 | 600.07 | 0.85 | 449.934 | 35.03 | 488.60 | 0.62 |
| 350.030 | 64.93 | 584.11 | 0.86 | 449.935 | 30.00 | 473.40 | 0.59 |
| 349.988 | 59.91 | 562.59 | 0.88 | 449.938 | 24.94 | 458.85 | 0.56 |
| 349.985 | 55.11 | 541.66 | 0.88 | 449.943 | 20.01 | 445.60 | 0.09 |
| 349.983 | 49.90 | 518.73 | 0.89 | 449.944 | 15.00 | 433.26 | 0.09 |
| 349.986 | 45.02 | 497.15 | 0.88 | 449.936 | 9.97 | 422.01 | 0.09 |
| 350.033 | 40.05 | 475.39 | 0.87 | 449.948 | 8.01 | 418.16 | 0.09 |
| 349.987 | 35.08 | 454.09 | 0.84 | 449.941 | 6.01 | 414.33 | 0.09 |
| 349.977 | 29.99 | 433.29 | 0.79 |  |  |  |  |
| 349.988 | 24.98 | 414.20 | 0.72 | 498.908 | 100.06 | 699.53 | 0.62 |
| 349.988 | 19.64 | 396.03 | 0.09 | 498.901 | 95.00 | 684.96 | 0.62 |
| 349.990 | 14.98 | 382.53 | 0.08 | 498.906 | 90.00 | 670.28 | 0.63 |
| 349.988 | 10.07 | 370.90 | 0.08 | 498.925 | 84.89 | 655.27 | 0.63 |
| 349.978 | 8.03 | 367.01 | 0.08 | 498.918 | 79.99 | 640.74 | 0.63 |
|  |  |  |  | 498.908 | 74.96 | 625.69 | 0.63 |
| 399.051 | 83.18 | 648.15 | 0.74 | 498.833 | 69.94 | 610.55 | 0.63 |
| 399.066 | 79.99 | 636.78 | 0.75 | 498.895 | 65.00 | 595.63 | 0.63 |
| 399.072 | 74.59 | 617.20 | 0.76 | 498.888 | 60.01 | 580.54 | 0.63 |
| 399.083 | 70.10 | 600.65 | 0.76 | 499.030 | 54.81 | 564.89 | 0.62 |
| 399.082 | 64.90 | 581.28 | 0.77 | 499.026 | 49.93 | 550.29 | 0.61 |
| 399.077 | 60.07 | 563.14 | 0.77 | 499.004 | 44.90 | 535.41 | 0.60 |
| 399.080 | 54.97 | 543.88 | 0.77 | 498.990 | 40.01 | 521.13 | 0.59 |
| 399.086 | 50.09 | 525.43 | 0.76 | 499.000 | 34.73 | 506.11 | 0.57 |
| 399.083 | 44.98 | 506.29 | 0.75 | 498.999 | 29.91 | 492.81 | 0.54 |
| 399.081 | 39.97 | 487.82 | 0.73 | 499.014 | 24.90 | 479.52 | 0.52 |
| 399.084 | 34.89 | 469.60 | 0.71 | 499.037 | 20.07 | 467.39 | 0.10 |
| 399.089 | 29.90 | 452.47 | 0.67 | 499.016 | 14.94 | 455.31 | 0.09 |
| 399.092 | 25.01 | 436.72 | 0.62 | 498.943 | 10.00 | 444.64 | 0.09 |
| 399.064 | 19.90 | 421.58 | 0.09 | 499.026 | 7.82 | 440.23 | 0.09 |
| 399.095 | 15.01 | 408.72 | 0.09 | 499.031 | 5.91 | 436.52 | 0.09 |
| 399.109 | 9.98 | 397.34 | 0.08 | 499.027 | 4.92 | 434.71 | 0.09 |

Standard uncertainties $u$ are $u(T)=0.03 \mathrm{~K}, u(p)=0.2 \mathrm{MPa}$ for $p \geq 20 \mathrm{MPa}$ and $u(p)=0.01 \mathrm{MPa}$ for $p \leq 20$ MPa where $u(p)$ contributed around $95 \%$ above 20 MPa and around $40 \%$ below 20 MPa to the combined uncertainty $u_{c}$.

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